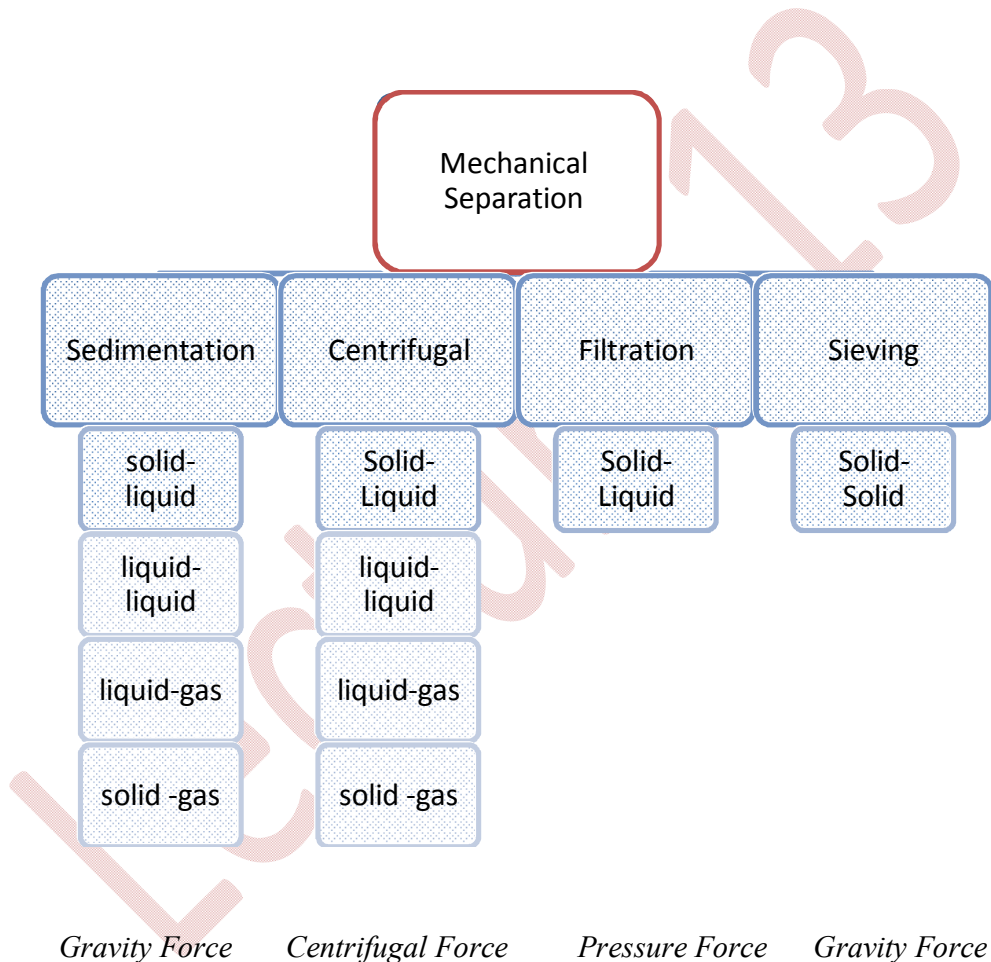


## MECHANICAL SEPARATIONS

**Mechanical separation** of particles from a fluid uses forces acting on these particles. So the separating action depends on the character of the particle being separated and the forces on the particle which cause the separation. Mechanical separations can be divided into four groups;



# UNIT OPERATION

## Sedimentation

### Introduction

In setting and sedimentation the particle are separated from the fluid by gravitational forces acting on the particles .

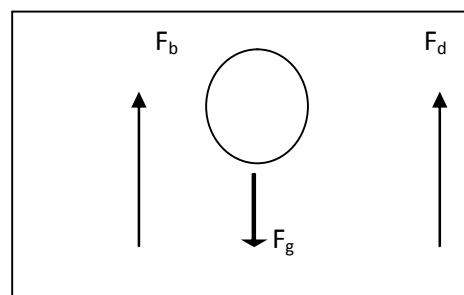
Free setting : when a particles is at a sufficient distance from the walls of the container and from other particles so that its fall is not affected by then .( The ratio of the particle dia. to the container dia. is less than 1/200 or if the particle cen. is less than 0.2vol % in the solid ) .

Hindered setting : when the particles are crowded , the settle alower rate . The separation of a dilute slurry or suspension by gravity setting in a clear fluid and a slurry of higher solids content is called sedimentation .

### Gravitational sedimentation

#### Reminal falling ( setting ) velocity of a particle

Forces Balance :



gravitation Force = Bouyancy force + Dray force

$$F_g = F_b + F_d$$

## UNIT OPERATION

$$V_S \rho_s g = V_S \rho g + C_D A_{Proj} \cdot \frac{\rho U_t^2}{2}$$

$$V_S g (\rho_s - \rho) = C_D A_{Proj} \cdot \frac{\rho U_t^2}{2}$$

For spherical particle

$$V_S = \frac{\pi}{6} d_s^3$$

$$A_{proj} = \frac{\pi}{4} d_s^2$$

$$\frac{\pi}{6} d_s^3 g (\rho_s - \rho) = \frac{\pi}{4} d_s^2 C_D \cdot \frac{\rho U_t^2}{2}$$

$$U_t = \sqrt{\frac{4 d_s (\rho_s - \rho) g}{3 C_D \rho}}$$

terminal falling ( setting )

velocity of spherical particle

where :

$U_t$  : terminal falling velocity ( m/s )

$D_s$  : dia. of solid particle

$A_{proj}$  : projected area of solid particle (m<sup>2</sup>)

$\rho_s$  : density of solid ( kg / m<sup>3</sup> )

$\rho$  : density of fluid ( kg / m<sup>3</sup> )

$C_D$  : drag coeff.

$g$  : gravitational acc. ( m/ s<sup>2</sup> )

## UNIT OPERATION

In the deriving the terminal falling velocity eq. it has been ass.

- a) That the setting is not affected by the presence of other particles in the fluid ( i.e. free setting ) .
- b) The walls of the container a enatexert an appreciable retarding effect .
- c) The fluid can be considered as a continuous modia .

$C_D$  is a function of Reynolds num. of particle  $(Re)_p$  where :

$$(Re)_p = (\rho U_t d_s / \mu )$$

For a flow of  $(Re)_p < 0.2$  around a spherical particle stokes obtained the following formula from theoretical consideration

$$F_d = 3\pi d_s \mu U \quad \text{stokes law}$$

Where :

$$C_D A_{proj} \cdot \frac{\rho U_t^2}{2} = 3\pi d_s \mu U_t$$

$$C_D \cdot \frac{\pi}{4} d_s^2 \cdot \frac{\rho U_t^2}{2} = 3\pi d_s \mu U_t$$

$$C_D = \frac{24 \mu}{\rho U_t d_s} \rightarrow C_D = \frac{24}{(Re)_p} \quad \text{for } (Re)_p < 0.2$$

Sub. Interminal velocity eq. gives

$$U_t = \frac{d_s^2 (\rho_s - \rho) g}{18 \mu} \quad \left( \text{stokes eq. for steady streamline flow} \right. \\ \left. \text{past a sphere } (Re)_p < 0.2 \right)$$

## UNIT OPERATION

For non – spherical particle , the terminal falling velocity eq. can be written in the modified formas

$$U_t = \sqrt{\frac{4\phi d_s(\rho_s - \rho)g}{3C_D \rho}} \quad (\text{ for non-spherical particle } )$$

$\phi$  : sphericity