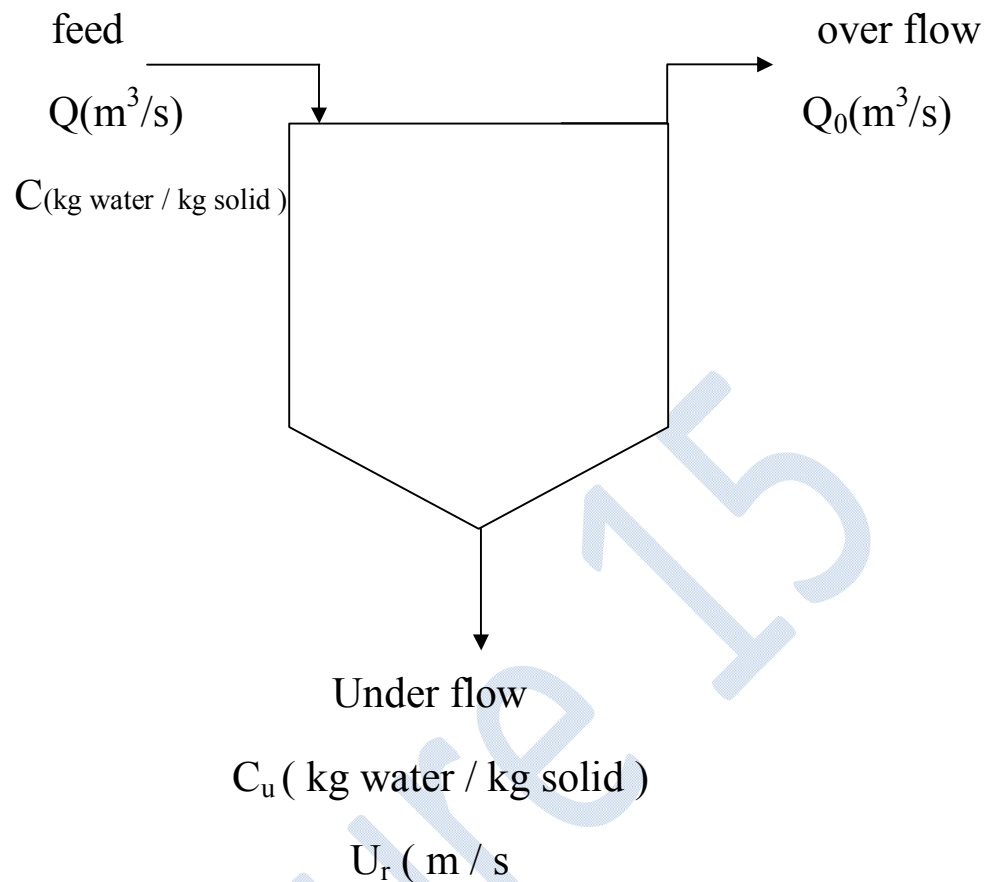


UNIT OPERATION



$$q = (U_c + U_r) A C_c \quad (1)$$

Where :

U_c : is the sedimentation velocity at cen. (C) in a batch sys.

In the under flow , the corresponding relation is

$$q = (U_u + U_r) A C_u \quad (2)$$

where :

C_u : is the cen. in the under flow

U_u : is the sedimentation velocity at a cen. C_u in a batch sys.

From eq.(2)

UNIT OPERATION

$$U_r = \frac{q}{AC_u} - U_u \quad (3)$$

Sub. In eq. (1) :

$$q = (U_c + \frac{q}{AC_u} - U_u)A_c$$

$$\frac{q}{A} = \frac{U_c - U_u}{\left(\frac{1}{c}\right) - \left(\frac{1}{c_u}\right)} \quad (4)$$

If the sedimentation rate in the under flow is small compared with that in the settling zone (i.e. $U_u \ll U_c$)

$$\frac{q}{A} = \frac{U_c c}{1 - \left(\frac{c}{c_u}\right)} \quad (5)$$

Thus if suspension of cen. (C) is fed to the tank at a volumetric rate Q :

$$\text{Solid input} = Q_c = \frac{AU_c c}{1 - \left(\frac{c}{c_u}\right)} \quad \text{eq. (5)}$$

Thus

$$\left(\frac{c}{c_u}\right) = 1 - \frac{U_c A}{Q} \quad (6)$$

The liq. Flow rate in the overflow Q_0 is the difference between the feed rate to the thickener and the rate at which solids with under flow

Thus :

$$Q_0 = Q(1 - C) - Q_c \left(\frac{1 - c_u}{c_u}\right) \quad \text{or} \quad \frac{Q_0}{Q} = 1 - \frac{c}{c_u}$$

From eq. (6)

$$A = \frac{Q}{U_c} \left(1 - \frac{c}{c_u}\right) \quad \text{area of thickener} \quad (8)$$

UNIT OPERATION

Interns of the mass ratio of liq. To solid in the feed (Y) and the corresponding value (U) in the under flow

$$Y = \left(\frac{1-C}{C} \right) \frac{\rho}{\rho_s} \quad \text{and} \quad U = \left(\frac{1-C_u}{C_u} \right) \frac{\rho}{\rho_s}$$

Then

$$C = \frac{1}{1+Y\left(\frac{\rho_s}{\rho}\right)}, \quad C_u = \frac{1}{1+U\left(\frac{\rho_s}{\rho}\right)}$$

and

$$A = \frac{Q}{U_c} \left[1 - \frac{1+U\left(\frac{\rho_s}{\rho}\right)}{1+Y\left(\frac{\rho_s}{\rho}\right)} \right]$$

$$A = \frac{Q(Y-U)\rho_s}{U_c \rho}$$

The value of (A) should be calculated for the whole range of cen.s present in the thickener and the design should then be based on the max. value so obtained .

EXAMPLE

A continuous separating tank is to be designed to follow after a water washing plant for liquid oil. Estimate the necessary area for the tank if the oil, on leaving the washer , is in the form of globules 5.1×10^{-5} m diameter , the feed concentration is 4 kg water to 1 kg oil , and the leaving water is effectively oil free . The feed rate is 1000 kg/h , the density of the oil is 894 kg/m^3 and the temperature of the oil and of the water is 38°C . Assume Stokes' Law .

Viscosity of water = $0.7 \times 10^{-3} \text{ N s/m}^2$

Density of water = 1000 kg/m^3

UNIT OPERATION

Diameter of globules = 5.1×10^{-5} m

$$V_m = \frac{D_p^2 g (\rho_p - \rho_c)}{18\mu}$$

$$V_m = (5.1 \times 10^{-5})^2 \times 9.81 \times (1000 - 894) / (18 \times 0.7 \times 10^{-3})$$

$$V_m = 2.15 \times 10^{-4} \text{ m/s} = 0.77 \text{ m/h}$$

since $F = 4$ and $U = 0$,

Q = flow of minor component = $1000/5 = 200$ kg/h ;

$$A = 4 \times 200 / (0.77 \times 1000) = 1.0 \text{ m}^2$$